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(54) RARE EARTH ALLOY POWDER FOR PERMANENT MAGNET AND METHOD FOR MANUFACTURING RARE EARTH PERMANENT MAGNET**(57)Abstract:**

PROBLEM TO BE SOLVED: To provide a method to add Co, Cu, Dy, etc. to rare earth alloy permanent magnetic powder material which can fully utilize the conventional rare earth material alloy with no change to it, achieving a high magnetic properties but causing neither generation of coarse grain growth nor reduction in coercive force when it is sintered later on.

SOLUTION: This invention relates to production methods for rare earth alloy powder and for permanent magnets using the powder. For the rare earth alloy powder, the first alloy group is defined to contain 29-33 mass % of R (the rare earth element(s) containing at least one or more of rare earth elements, including Y), 0.8-1.2 mass % of B, a combination of 0.01-0.5 mass % of Ga and 0.01-2.0 mass % of Al added for compound effect, and remainder being Fe, and the second alloy group is defined to contain 29-33 mass % of R (the rare earth element(s) containing at least one or more of rare earth elements, including Y), a combination of 0.01-0.5 mass % of Ga and 0.01-2.0 mass % of Al added for compound effect, and remainder being Fe (A part of Fe can be replaced by Co and Cu). This invention features production methods for rare earth alloy powder mixed of the first and second alloy group powders and for permanent magnets using the powder.

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(54) 【発明の名称】 希土類永久磁石用合金粉末および希土類永久磁石の製造方法

(57) 【要約】

【課題】 本発明は、Co、Cu、Dy等を添加する方法において、従来の希土類量原料合金を何ら変更することなく十分活用でき、かつ焼結時の粗大結晶粒の発生および保磁力の低下を招来せず、高い磁気特性を達成することを目的とする。

【解決手段】 本発明は、R (Yを含む希土類元素の少なくとも1種以上) 29~33mass%、硼素B 0.8~1.2mass%、GaとAlを複合添加してGa 0.01~0.5mass%及びAl 0.01~2.0mass%、残部Feからなる合金を第1合金とし、R (Yを含む希土類元素の少なくとも1種以上) 29~33mass%、GaとAlを複合添加してGa 0.01~0.5mass%及びAl 0.01~2.0mass%、残部Fe (Feの一部をCoおよびCuで置換したもの) からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末、それを用いた希土類永久磁石の製造方法である。

【特許請求の範囲】

【請求項 1】 R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8~1.2mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、

R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、

第 1 合金粉末と第 2 合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末。

【請求項 2】 Cu と Co の重量比が $Cu/Co=0.02\sim0.2$ であることを特徴とする請求項 1 記載の希土類合金粉末。

【請求項 3】 前記 R のうち重希土類の含有量が異なる第 1 合金粗粉、並びに硼素 B 量の異なる第 1 合金粗粉の第 1 合金粉末の 2 種以上と、第 2 合金粉末が、所定組成に混合されていることを特徴とする請求項 1 記載の希土類合金粉末。

【請求項 4】 R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8~1.2mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、

R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、

第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、

次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 5】 R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8~1.2mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、

R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換し、Cu と Co の重量比が $Cu/Co=0.02\sim0.2$) からなる合金を第 2 合金とし、第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、

次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 6】 R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8~1.2mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe からなる合金であって、前記 R のうち重希土類の含有量が異なる第 1 合金粗粉、並びに硼素 B 量の異なる第 1 合金粗粉の第 1 合金粉末の 2 種以上を第 1 合金とし、

R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、

第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、

次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 7】 R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8~1.2mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、

R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8mass% 未満、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、

第 1 合金粉末と第 2 合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末。

【請求項 8】 Cu と Co の重量比が $Cu/Co=0.02\sim0.2$ であることを特徴とする請求項 7 記載の希土類合金粉末。

【請求項 9】 前記 R のうち重希土類の含有量が異なる第 1 合金粗粉、並びに硼素 B 量の異なる第 1 合金粗粉の第 1 合金粉末の 2 種以上と、

第 2 合金粉末が、所定組成に混合されていることを特徴とする請求項 7 記載の希土類合金粉末。

【請求項 10】 R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8~1.2mass%、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、

R (Y を含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B0.8mass% 未満、Ga と Al を複合添加して GaO.01~0.5mass% 及び AlO.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、

第 1 合金粉末と第 2 合金粉末が所定組成に混合された希

土類合金粉末を磁場中で成形し、
次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 11】 R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8~1.2mass%、Ga と Al を複合添加して Ga 0.01~0.5mass% 及び Al 0.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、
R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8mass% 未満、Ga と Al を複合添加して Ga 0.01~0.5mass% 及び Al 0.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換し、Cu と Co の重量比が Cu/Co=0.02~0.2) からなる合金を第 2 合金とし、
第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、
次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 12】 R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8~1.2mass%、Ga と Al を複合添加して Ga 0.01~0.5mass% 及び Al 0.01~2.0mass%、残部 Fe からなる合金であって、前記 R のうち重希土類の含有量が異なる第 1 合金粗粉、並びに硼素 B 量の異なる第 1 合金粗粉の第 1 合金粉末の 2 種以上を第 1 合金とし、
R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8mass% 未満、Ga と Al を複合添加して Ga 0.01~0.5mass% 及び Al 0.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、
第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、
次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 13】 R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8~1.2mass%、Al 0.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、
R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、Al 0.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、
第 1 合金粉末と第 2 合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末。

【請求項 14】 Cu と Co の重量比が Cu/Co=0.02~0.2 であることを特徴とする請求項 13 記載の希土類合金粉末。

【請求項 15】 前記 R のうち重希土類の含有量が異なる第 1 合金粗粉、並びに硼素 B 量の異なる第 1 合金粗粉の第 1 合金粉末の 2 種以上と、
第 2 合金粉末が、所定組成に混合されていることを特徴とする請求項 13 記載の希土類合金粉末。

【請求項 16】 R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8~1.2mass%、Al 0.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、
R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、Al 0.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、
第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、
次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 17】 R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8~1.2mass%、Al 0.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、
R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、Al 0.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換し、Cu と Co の重量比が Cu/Co=0.02~0.2) からなる合金を第 2 合金とし、
第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、
次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 18】 R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8~1.2mass%、Al 0.01~2.0mass%、残部 Fe からなる合金であって、前記 R のうち重希土類の含有量が異なる第 1 合金粗粉、並びに硼素 B 量の異なる第 1 合金粗粉の第 1 合金粉末の 2 種以上を第 1 合金とし、
R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、Al 0.01~2.0mass%、残部 Fe (Fe の一部を Co および Cu で置換したもの) からなる合金を第 2 合金とし、
第 1 合金粉末と第 2 合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、
次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項 19】 R (Yを含む希土類元素の少なくとも 1 種以上) 29~33mass%、硼素 B 0.8~1.2mass%、Al 0.01~2.0mass%、残部 Fe からなる合金を第 1 合金とし、

R (Yを含む希土類元素の少なくとも 1 種以上) 29~

33mass%、硼素B0.8mass%未満、Al0.01~2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、

第1合金粉末と第2合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末。

【請求項20】 CuとCoの重量比がCu/Co=0.02~0.2であることを特徴とする請求項19記載の希土類合金粉末。

【請求項21】 前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上と、

第2合金粉末が、所定組成に混合されていることを特徴とする請求項19記載の希土類合金粉末。

【請求項22】 R（Yを含む希土類元素の少なくとも1種以上）29~33mass%、硼素B0.8~1.2mass%、Al0.01~2.0mass%、残部Feからなる合金を第1合金とし、

R（Yを含む希土類元素の少なくとも1種以上）29~33mass%、硼素B0.8mass%未満、Al0.01~2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、

第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、

次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項23】 R（Yを含む希土類元素の少なくとも1種以上）29~33mass%、硼素B0.8~1.2mass%、Al0.01~2.0mass%、残部Feからなる合金を第1合金とし、

R（Yを含む希土類元素の少なくとも1種以上）29~33mass%、硼素B0.8mass%未満、Al0.01~2.0mass%、残部Fe（Feの一部をCoおよびCuで置換し、CuとCoの重量比がCu/Co=0.02~0.2）からなる合金を第2合金とし、

第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、

次いで焼結することを特徴とする希土類永久磁石の製造方法。

【請求項24】 R（Yを含む希土類元素の少なくとも1種以上）29~33mass%、硼素B0.8~1.2mass%、Al0.01~2.0mass%、残部Feからなる合金であって、前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上を第1合金とし、

R（Yを含む希土類元素の少なくとも1種以上）29~33mass%、硼素B0.8mass%未満、Al

0.01~2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、

第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、

次いで焼結することを特徴とする希土類永久磁石の製造方法。

【発明の詳細な説明】

【0001】

【発明が属する技術分野】本発明は、R-T-B（Rは希土類、Tは遷移金属など、Bは硼素）系永久磁石用合金粉末と、これを用いたR-T-B系永久磁石の製造方法に関する。

【0002】

【従来の技術】今日、R-T-B系永久磁石は各種家電製品、情報通信機器、コンピュータ周辺機器、各種モータといった幅広い分野で使用され、これら製品群の小型化、高速化および使用環境の拡大に合わせて、用いられる磁石も、磁気特性、耐熱性、耐食性の更なる向上が望まれている。

【0003】R-T-B系永久磁石は、原料合金を溶解し、得られたインゴットを粉砕、成形、焼結、熱処理、加工して製造される。粉砕はボールミル等を用いた湿式粉砕も可能であるが、不活性高圧ガスを用いたジェットミル粉砕が一般的である。このようにして得られる微粉は極めて活性であるため、ジェットミルの粉砕気流中に微量の酸素を混合して安定化を図ったり、または鉱物油などに微粉を回収する方法が採られている。磁場中で行なう成形は、乾式成形、湿式成形いずれも用いられている。焼結は、1000℃~1150℃の温度範囲で真空中あるいは不活性ガス中で行われ、次いで得られた焼結体は適当な温度で1回または複数回の熱処理を施すのが一般的である。

【0004】R-T-B系永久磁石は、当初は耐食性、耐熱性が低いという問題があったが、添加元素の検討、メッキ等のコーティング技術の発展により著しく改善されてきた。また、磁石素材そのものの耐食性改善も、コーティング後の信頼性を高める上で極めて重要であり、種々の添加元素が検討されている。これらの添加元素としてCo、Dyといった元素が一般的に用いられている。Coはキュリー温度を上昇させ温度特性を改善し、またリッチ相をR₃Co金属間化合物とすることにより耐食性を改善する。Dyは主相の異方性磁界H_Aを増加させることにより保磁力を向上させる。さらにCu、Ga、Alといった微量添加元素も用いられている。CuはCoと複合添加することにより最適熱処理範囲を広げ、かつ保磁力向上に寄与する（特開平1-219143）。また、Cuの添加により粒界相がR-Co-Cu金属間化合物になりCo添加のみの場合に比べ、更に耐食性が増すことが知られている。Ga、Al等の添加元

素も保磁力の向上に効果があることが知られている。

【0005】Co、Dy、Cu等の添加方法としては、原料合金の溶解段階で添加する、いわゆる1合金法と、所定組成の合金を、粗粉碎後または微粉碎後に混合する2合金法（混合法）が用いられている。2合金法では粉末の酸化防止を目的に、Co、Dyといった耐食性に寄与する元素をRリッチな合金に添加し、特に、Rリッチ合金を特定の結晶構造を持った金属間化合物とすることにより、合金粉末の耐酸化性が増すことが示されている（特開平5-182813～182816）。また、保磁力の向上に寄与する、Cu、Al、Gaなどの元素を粒界相に集中させることを意図し、これらの元素をRリッチ合金側へ添加する方法が示されている。

【0006】

【発明が解決しようとする課題】Co、Dy、Cu等の添加は耐食性、耐熱性の改善に効果があるが、1合金法を用いた場合、CoおよびCuを添加すると、高い残留磁束密度が要求されるDyの少ない組成域において、焼結時の粒成長が起りやすく、粗大結晶粒が多く現れる傾向にある。その結果、焼結体の主相結晶粒の粒径分布が広くなり、保磁力、角型性の低下を招きやすいという問題があった。また、2合金法は高性能化の観点から大変魅力的な方法であるが、これを量産規模で実施しようとすると次のような問題点があげられる。すなわち、希土類量の少ない主相合金と希土類に富んだいわゆるRリッチ合金を用意せねばならず、原料合金系の大幅な変更が求められる。また、主相合金とRリッチ合金は水素吸蔵特性が異なるために粗粉碎条件の変更が必要であり、また微粉碎性が異なるために混合粗粉をジェットミル粉碎する場合、Rリッチ合金が飛散しやすく、また微粉碎後に混合する場合は、それぞれの粉碎条件を別個最適化しなければならないだけでなく、工程が複雑になってしまう。

【0007】本発明は、Co、Cu、Dy等を添加する方法において、従来の希土類量原料合金を何ら変更することなく十分活用でき、かつ焼結時の粗大結晶粒の発生および保磁力の低下を招来せず、高い磁気特性を達成することができるR-T-B系永久磁石用合金粉末およびR-T-B系永久磁石の製造方法を提供することを目的とする。

【0008】

【課題を解決するための手段】本発明は、上記の課題を解決するために、下記の構成を主旨とする。なお、下記（1）～（6）は、GaとAlの複合添加効果を利用して、第2合金の硼素B添加量を実質的にゼロとした場合である。下記（7）～（12）は、GaとAlの複合添加効果を利用して、第2合金の硼素B添加量を0.8mass%未満とした場合である。また、下記（13）～（18）は、Alを単独添加して第2合金の硼素B添加量を実質的にゼロとした場合である。下記（19）～

（24）は、Alを単独添加して、第2合金の硼素B添加量を0.8mass%未満とした場合である。

（1）R（Yを含む希土類元素の少なくとも1種以上）29～33mass%、硼素B0.8～1.2mass%、GaとAlを複合添加してGa0.01～0.5mass%及びAl0.01～2.0mass%、残部Feからなる合金を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）29～33mass%、GaとAlを複合添加してGa0.01～0.5mass%及びAl0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末である。

（2）CuとCoの重量比がCu/Co=0.02～0.2であることを特徴とする（1）記載の希土類合金粉末である。

（3）前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上と、第2合金粉末が、所定組成に混合されていることを特徴とする（1）記載の希土類合金粉末である。

（4）R（Yを含む希土類元素の少なくとも1種以上）29～33mass%、硼素B0.8～1.2mass%、GaとAlを複合添加してGa0.01～0.5mass%及びAl0.01～2.0mass%、残部Feからなる合金を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）29～33mass%、GaとAlを複合添加してGa0.01～0.5mass%及びAl0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

（5）R（Yを含む希土類元素の少なくとも1種以上）29～33mass%、硼素B0.8～1.2mass%、GaとAlを複合添加してGa0.01～0.5mass%及びAl0.01～2.0mass%、残部Feからなる合金を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）29～33mass%、GaとAlを複合添加してGa0.01～0.5mass%及びAl0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換し、CuとCoの重量比がCu/Co=0.02～0.2）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

（6）R（Yを含む希土類元素の少なくとも1種以上）

29~33mass%、硼素B0.8~1.2mass%、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Feからなる合金であって、前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上を第1合金とし、R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Fe(Feの一部をCoおよびCuで置換したもの)からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(7) R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、硼素B0.8~1.2mass%、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Feからなる合金を第1合金とし、R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、
10 硼素B0.8mass%未満、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Fe(Feの一部をCoおよびCuで置換したもの)からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末である。

(8) CuとCoの重量比が $Cu/Co=0.02\sim0.2$ であることを特徴とする(7)記載の希土類合金粉末である。

(9) 前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上と、第2合金粉末が、所定組成に混合されていることを特徴とする(7)記載の希土類合金粉末である。

(10) R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、硼素B0.8~1.2mass%、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Feからなる合金を第1合金とし、R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、
20 硼素B0.8mass%未満、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Fe(Feの一部をCoおよびCuで置換したもの)からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(11) R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、硼素B0.8~1.2mass%

ss%、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Feからなる合金を第1合金とし、R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、
30 硼素B0.8mass%未満、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Fe(Feの一部をCoおよびCuで置換したもの)からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(12) R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、硼素B0.8~1.2mass%、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Feからなる合金であって、前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上を第1合金とし、R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、
40 硼素B0.8mass%未満、GaとAlを複合添加してGa0.01~0.5mass%及びAl0.01~2.0mass%、残部Fe(Feの一部をCoおよびCuで置換したもの)からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(13) R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、硼素B0.8~1.2mass%、Al0.01~2.0mass%、残部Feからなる合金を第1合金とし、R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、Al0.01~2.0mass%、
50 残部Fe(Feの一部をCoおよびCuで置換したもの)からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末である。

(14) CuとCoの重量比が $Cu/Co=0.02\sim0.2$ であることを特徴とする(13)記載の希土類合金粉末である。

(15) 前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上と、第2合金粉末が、所定組成に混合されていることを特徴とする(13)記載の希土類合金粉末である。

(16) R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、硼素B0.8~1.2mass%、Al0.01~2.0mass%、残部Feからなる合金を第1合金とし、R(Yを含む希土類元素の少なくとも1種以上)29~33mass%、Al0.

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0.1～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(17) R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8～1.2mass%、Al 0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換し、CuとCoの重量比がCu/Co=0.02～0.2）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(18) R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8～1.2mass%、Al 0.01～2.0mass%、残部Feからなる合金であって、前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、Al 0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(19) R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8～1.2mass%、Al 0.01～2.0mass%、残部Feからなる合金を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8mass%未満、Al 0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合されていることを特徴とする希土類合金粉末である。

(20) CuとCoの重量比がCu/Co=0.02～0.2であることを特徴とする(19)記載の希土類合金粉末である。

(21) 前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上と、第2合金粉末が、所定組成に混合されていることを特徴とする(19)記載の希土類合金粉末である。

(22) R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8～1.2mass%、Al 0.01～2.0mass%、残部Feか

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らなる合金を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8mass%未満、Al 0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(23) R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8～1.2mass%、Al 0.01～2.0mass%、残部Feからなる合金を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8mass%未満、Al 0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換し、CuとCoの重量比がCu/Co=0.02～0.2）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

(24) R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8～1.2mass%、Al 0.01～2.0mass%、残部Feからなる合金であって、前記Rのうち重希土類の含有量が異なる第1合金粗粉、並びに硼素B量の異なる第1合金粗粉の第1合金粉末の2種以上を第1合金とし、R（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、硼素B 0.8mass%未満、Al 0.01～2.0mass%、残部Fe（Feの一部をCoおよびCuで置換したもの）からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合された希土類合金粉末を磁場中で成形し、次いで焼結することを特徴とする希土類永久磁石の製造方法である。

【0009】（作用）この発明は上記問題点を解決する手段として、2合金法における、Co、Cu、Dy、Bの添加方法および希土類量を検討した結果、Co、Cuを含まない従来希土類量の合金粗粉を第1合金とし、これに、第1合金と基本的に希土類量は等しく、Bを実質的に含まないか、または第1合金よりも少ない第2合金に特定比率のCo、Cuを添加し、これらの合金粗粉を混合後微粉碎、焼結することにより、従来の希土類量原料合金を何ら変更することなく十分活用でき、かつ焼結時の粗大結晶粒の発生および保磁力の低下を招来せず、耐食性、耐熱性の向上および高い磁気特性を達成することができることを見出したものである。さらに、Dy、B等の組成の異なる複数の合金粗粉を第2合金と混合する方法により、混合比を変えるだけで成分調整が容易に行なえることを見出したものである。

【0010】すなわち、この発明はR（Yを含む希土類元素の少なくとも1種以上）2.9～3.3mass%、B

0.8~1.2mass%、Al 0.01~2.0mass%、残部Feおよび不可避不純物からなる合金を第1合金とし、第1合金と実質的に等しいR量、B 0.8mass%未満、Al 0.01~2.0mass%、残部Fe (Feの一部をCoおよびCuで置換したもの) および不可避不純物からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合されているR-T-B系合金粉末である。また、R (Yを含む希土類元素の少なくとも1種以上) 29~33mass%、B 0.8~1.2mass%、Al 0.01~2.0mass%、Ga 0.01~0.5mass%、残部Feおよび不可避不純物からなる合金を第1合金とし、第1合金と実質的に等しいR量、B 0.8mass%未満、Al 0.01~2.0mass%、Ga 0.01~0.5mass%、残部Fe (Feの一部をCoおよびCuで置換したもの) および不可避不純物からなる合金を第2合金とし、第1合金粉末と第2合金粉末が所定組成に混合されているR-T-B系合金粉末である。また、CuとCoの重量比がCu/Co=0.02~0.2である上記R-T-B系合金粉末である。また、重希土類量の異なる第1合金粉末2種以上と第2合金粉末が、所定組成に混合されているR-T-B系合金粉末である。更に、これらのR-T-B系合金粉末を磁場中で成形し、次いで焼結するR-T-B系永久磁石の製造方法である。

【0011】

【発明の実施の形態】この発明において、RはYを含む希土類元素の少なくとも1種以上で、Nd、Pr、Dyが好ましい。Nd、Dyのみでも良いがNd、Prの混合物をNdの代わりに用いても良い。主体となる第1合金のRは、29mass%未満では液相が不足するために焼結不良となり、33mass%を超えると残留磁束密度が低下するため、添加量は29mass%~33mass%とする。第1合金のBは0.8mass%未満ではR₂T₁₇相が出現するために保磁力が急減し、1.2mass%を超えると非磁性相であるBリッチ相が多くなりすぎてしまい残留磁束密度が低下するので0.8~1.2mass%とする。第1合金にAlまたはAl、Gaを添加する場合、Al、Ga量はAl 0.01~2.0mass%、Ga 0.01~0.5mass%とする。Alは保磁力向上の効果を示すが、0.01mass%未満ではその効果が十分ではなく2.0mass%を超えると残留磁束密度の低下が大きく好ましくない。Gaも同様にその添加によって保磁力が向上するが、やはり0.01mass%未満ではその効果が不十分であり、0.5mass%を超えると保磁力向上の効果が飽和するとともに残留磁束密度が低下する。本発明においてGaとAlは複合添加すると、より効果的である。

【0012】第2合金のRは基本的には第1合金と等し

くするが、合金調達の都合やロットバラツキ等で多少ずれてもかまわない。組成範囲は第1合金と等しくR 29~33mass%とする。第2合金のB量は0.8mass%以上では、粗大粒の発生を抑制する効果が小さくなってしまい保磁力の減少、角型性の悪化を招く。したがって0.8mass%未満とするが、好ましくはBを添加しない。第2合金のGa、Alは基本的には第1合金と等しくするが、合金調達の都合やロットバラツキ等で多少ずれてもかまわない。AlまたはAl、Gaを添加する場合、組成範囲は第1合金と等しくAl 0.01~2.0mass%、Ga 0.01~0.5mass%とする。なお、本発明においてGaとAlは複合添加すると、より効果的である。第2合金のCo、Cuの添加量は特に限定されず、最終組成における添加量と配合比の関係から設定でき、最終組成における添加量は用途、目的に応じて設定できる。一方、第1合金に対する第2合金の配合比は、第1合金：第2合金=99：1~70：30が好ましいが、これも特に限定はされない。

【0013】CuとCoの重量比はCu/Coが0.02未満であると熱処理温度範囲を広げる効果が小さく、0.2を超えると、Coが2mass%程度のごく一般的な組成において、残留磁束密度の低下、角型性の低下を招く。したがってCu/Co=0.02~0.2とする。

【0014】本発明における第1合金粗粉は単一組成のものに限らない。すなわち、Dy、Tbなどの重希土類量が異なる第1合金粗粉、更にB量の異なる第1合金粗粉、これら2種以上に対して、Co、Cuの添加された第2合金粗粉を配合し混合しても良い。この場合、DyやBの調整は配合比を変えるだけで簡単に行なうことができる。

【0015】

【実施例】以下、本発明の具体的実施例を示し、本発明の内容を詳細に説明する。

(実施例1) Nd 25.3mass%、Pr 7.0mass%、B 1.0mass%、Al 0.07mass%、残部Feよりなる合金をストリップキャスト法で铸造した。この合金を処理容器に装入し、真空中で1000℃×2hの熱処理を施した後、水素吸蔵法により解砕して原料粗粉とした(表1記載、合金A)。また、Nd 18.6mass%、Pr 5.2mass%、Dy 8.5mass%、Co 20mass%、Cu 1mass%、Al 0.07mass%、残部Feからなる合金も同様にして原料粗粉とした(表1記載、合金I)。この2種類の合金粗粉を合金A 90mass%、合金I 10mass%の割合でV型混合機に投入し、15分間混合した。この混合粗粉を窒素高圧ガスをういたジェットミルにて、平均粒径4.7μmとなるように粉碎した。得られた混合微粉を0.6MA/mの磁場中で配向させながら、1.0Tonn/cm²の圧力で成形した。得られた成形体

は、真空中にて1060℃、1080℃、または1100℃×2時間の焼結を行なった。次いで、これらの焼結体は、Ar雰囲気中で900℃×1時間の熱処理を施した後、さらに480℃×1時間の熱処理を施した。焼結体の外観を観察後、磁気特性を測定した。最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。磁気特性は良好な値が得られ、このとき焼結温度は1100℃であり、また粗大粒などは見られなかった。

【0016】(比較例1)本実施例の最終組成である、Nd24.6mass%、Pr6.85mass%、Dy0.85mass%、B0.9mass%、Co2mass%、Cu0.1mass%、Al0.07mass%、残部Feよりなる合金をストリップキャスト法で鑄造し、実施例1と同様に粉碎、焼結、熱処理を行なった。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。1060℃、1080℃、1100℃のうち最適な焼結温度は1080℃であったが、Hcjが実施例1よりも低く、また粗大粒が観察された。また、1060℃の試料は明らかに焼結不足であった。

【0017】(比較例2)表1に示した合金Rと合金Sを用いて実施例1と同様に粗粉碎し、最終組成となるよう混合後、微粉碎、焼結、熱処理を行なった。ここで、Co、Cuは両合金に様に添加し、Dyは合金Sに添加した。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。Hcjが実施例1よりも低く、また粗大粒が観察された。

【0018】(比較例3)表1に示した合金Cと合金Qを用いて実施例1と同様に粗粉碎し、最終組成となるよう混合後、微粉碎、焼結、熱処理を行なった。ここで、Dy、Co、Cuは合金Qに添加し、Bは両合金とも一様に添加した。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。Hcjが実施例1よりも低く、また粗大粒は比較例1、2より少ないが観察された。

【0019】(実施例2)表1に示した合金Aと合金Kを用いて実施例1と同様に粗粉碎し、最終組成となるよう混合後、微粉碎、焼結、熱処理を行なった。ここで、Dy、Co、Cuは合金Kに添加しBは0.4mass%とした。合金Kは本発明の第2合金である。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。磁気特性は実施例1と同様に良好な値が得られ、このとき焼結温度は1100℃であり、また粗大粒などは見られなかった。

【0020】(実施例3)表1に示した合金Aと合金L

を用いて実施例1と同様に粗粉碎し、最終組成となるよう混合後、微粉碎、焼結、熱処理を行なった。ここで、Dy、Co、Cuは合金Lに添加しBは0.7mass%とした。合金Lは本発明の第2合金である。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。磁気特性は実施例1と同様に良好な値が得られ、このとき焼結温度は1100℃であり、また粗大粒などは見られなかった。

【0021】(実施例4)表1に示した合金Bと合金Cと合金Iを用いて実施例1と同様に粗粉碎し、最終組成となるよう混合後、微粉碎、焼結、熱処理を行なった。ここで、Dy、Co、Cuは合金Iに添加しBは無添加とした。合金Iは本発明の第2合金である。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。磁気特性は実施例1と同様に良好な値が得られ、このとき焼結温度は1100℃であり、また粗大粒などは見られなかった。

【0022】(実施例5)表1に示した合金Bと合金Cと合金Dと合金Jを用いて実施例1と同様に粗粉碎し、最終組成となるよう混合後、微粉碎、焼結、熱処理を行なった。ここで、Co、Cuは合金Jに添加しBは無添加とした。合金Jは本発明の第2合金である。Dyは本発明の第1合金の一つである合金Dにより添加した。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。磁気特性は実施例1と同様に良好な値が得られ、このとき焼結温度は1100℃であり、また粗大粒などは見られなかった。

【0023】(比較例4)表1に示した合金Tと合金Uを用いて実施例1と同様に粗粉碎し、最終組成となるよう混合後、微粉碎、焼結、熱処理を行なった。ここで、Dy、Co、CuはRリッチな合金Uに添加しBは無添加とした。合金Uは本発明の第2合金ではない。得られた焼結体の外観を観察後、磁気特性を測定し、最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表1に示す。磁気特性は実施例1と同様に良好な値が得られ、このとき焼結温度は1100℃であり、また粗大粒などは見られなかった。この結果から、実施例1～5で得られる磁気特性は、従来の2合金法(比較例4)と同等のものであることが分かる。

【0024】(実施例6～10、比較例5～8)第1合金A～D、第2合金I～L、比較用合金P～Uの組成において、Gaを0.1mass%添加した合金を新たに作製し、第1合金A'～D'、第2合金I'～L'、比較用合金P'～U'とした。実施例1～5、比較例1～4と同様の方法で焼結体を作製し、焼結体の外観を観察後、磁気特性を測定した。最も角型性の高い場合の磁気特性、焼結温度および外観観察の結果を表2に示す。最

適焼結温度、粗大粒の外観に関しては表1の結果と同様であるが、Hc_jの水準は0.2MA/m程度向上することが確認できる。Gaの複合添加効果が出ている。

*【0025】

【表1】

		組 成 (mass%)							
		Nd	Pr	Dy	TRE	B	Co	Cu	Fe
第1合金	A	25.3	7.0	0	32.3	1.00	0	0	bal.
	B	25.2	7.0	0	32.2	1.07	0	0	bal.
	C	25.3	7.0	0	32.3	0.90	0	0	bal.
	D	11.9	3.3	17.0	32.2	1.07	0	0	bal.
第2合金	I	18.6	5.2	8.5	32.3	0	20	1	bal.
	J	25.3	7.0	0	32.3	0	20	1	bal.
	K	20.8	5.7	5.7	32.2	0.4	13.3	0.67	bal.
	L	23.1	6.4	2.8	32.3	0.7	6.7	0.34	bal.
比較合金	P	24.6	6.85	0.85	32.3	0.90	2	0.1	bal.
	Q	18.5	5.2	8.5	32.2	0.90	20	1	bal.
	R	25.3	6.9	0	32.2	0.90	2	0.1	bal.
	S	12.0	3.3	17.0	32.3	1.07	2	0.1	bal.
	T	23.8	6.6	0	30.4	1.03	0	0	bal.
最終組成		24.6	6.85	0.85	32.3	0.90	2	0.1	bal.

Al:0.06~0.08mass%

	配合(合金×配合率)	Br (T)	Hc _j (MA/)	Hk/Hc (%)	最適焼 温度	粗大粒 外観
実施例	A×0.9+I×0.1	1.36	1.17	98.3	1100	○
比較例	P	1.35	1.01	98.1	1080	×
比較例	R×0.95+S×0.05	1.35	1.0	98.2	1080	×
比較例	C×0.9+Q×0.1	1.35	1.03	98.1	1080	△
実施例	A×0.85+K×0.15	1.35	1.16	98.0	1100	○
実施例	A×0.7+L×0.3	1.36	1.16	97.8	1100	○
実施例	B×0.53+C×0.37+I×0.1	1.35	1.17	98.2	1100	○
実施例	B×0.5+C×0.35+D×0.05+J	1.36	1.17	98.4	1100	○
比較例	T×0.88+U×0.12	1.36	1.18	98.1	1100	○

○:なし △:あり ×:多し

【0026】

【表2】

	配合(合金×配合率)	Br (T)	Hc _j (MA/)	Hk/Hc (%)	最適焼 温度	粗大粒 外観
実施例	A'×0.9+I'×0.1	1.35	1.38	98.4	1100	○
比較例	P'	1.34	1.21	97.9	1080	×
比較例	R'×0.95+S'×0.05	1.35	1.22	97.9	1080	×
比較例	C'×0.9+Q'×0.1	1.35	1.25	98.4	1080	△
実施例	A'×0.85+K'×0.15	1.35	1.37	98.2	1100	○
実施例	A'×0.7+L'×0.3	1.35	1.35	98.1	1100	○
実施例	B'×0.53+C'×0.37+I'×0.1	1.35	1.38	98.4	1100	○
実施例	B'×0.5+C'×0.35+D'×0.05+	1.36	1.37	98.4	1100	○
比較例	T'×0.88+U'×0.12	1.35	1.38	98.4	1100	○

○:なし △:あり ×:多し

【0027】

【発明の効果】本発明によれば、Co、Cu、Dy等を添加する方法において、従来の希土類量の原料合金を何

ら変更することなく十分活用でき、かつ焼結時の粗大結晶粒の発生および保磁力の低下を招来せず、高い磁気特性を達成することができる。

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(22)Date of filing : 27.07.2000 (72)Inventor : MOCHIZUKI MITSUAKI

(54) RARE EARTH ALLOY POWDER FOR RERMANENT MAGNET AND
METHOD FOR MANUFACTURING RARE EARTH PERMANENT MAGNET

(57)Abstract:

PROBLEM TO BE SOLVED: To provide a method to add Co, Cu, Dy, etc. to rare earth alloy permanent magnetic powder material which can fully utilize the conventional rare earth material alloy with no change to it, achieving a high magnetic properties but causing neither generation of coarse grain growth nor reduction in coercive force when it is sintered later on.

SOLUTION: This invention relates to production methods for rare earth alloy powder and for permanent magnets using the powder. For the rare earth alloy powder, the first alloy group is defined to contain 29-33 mass % of R (the rare earth element(s) containing at least one or more of rare earth elements, including Y), 0.8-1.2 mass % of B, a combination of 0.01-0.5 mass % of Ga and 0.01-2.0 mass % of Al added for compound effect, and remainder being Fe, and the second alloy group is defined to contain 29-33 mass % of R (the rare earth element(s) containing at least one or more of rare earth elements, including Y), a combination of 0.01-0.5 mass % of Ga and 0.01-2.0 mass % of Al added for compound effect, and remainder being Fe (A part of Fe can be replaced by Co and Cu). This invention features production methods for rare earth alloy powder mixed of the first and second alloy group powders and for permanent magnets using the powder.

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CLAIMS

[Claim(s)]

[Claim 1] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, Rare earth alloy powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by the 1st alloy powder and the 2nd alloy powder

being mixed by the predetermined presentation.

[Claim 2] Rare earth alloy powder according to claim 1 characterized by the weight ratio of Cu and Co being $Cu/Co=0.02-0.2$.

[Claim 3] Rare earth alloy powder according to claim 1 characterized by the 2nd alloy powder being mixed with two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, and the 1st alloy coarse powder with which the amounts of boron B differ in a list by the predetermined presentation.

[Claim 4] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 5] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe (a part of Fe is permuted by Co and Cu, and the weight ratio of Cu and Co is $Cu/Co=0.02-0.2$) is used as the 2nd alloy. The manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder

with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 6] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the alloy which consists of the remainder Fe, the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 7] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than [boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, Rare earth alloy powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by the 1st alloy powder and the 2nd alloy powder being mixed by the predetermined presentation.

[Claim 8] Rare earth alloy powder according to claim 7 characterized by the weight ratio of Cu and Co being $Cu/Co=0.02-0.2$.

[Claim 9] Rare earth alloy powder according to claim 7 characterized by the 2nd alloy powder being mixed with two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, and the 1st alloy coarse powder with which the amounts of boron B differ in a list by the predetermined presentation.

[Claim 10] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than [boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 11] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than [boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe (a part of Fe is permuted by Co and Cu, and the weight ratio of Cu and Co is $Cu/Co=0.02-0.2$) is used as the 2nd alloy. The manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 12] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the alloy which consists of the remainder Fe, the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than [boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 13] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Rare earth alloy powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu) aluminum0.01 - 2.0mass%, and is characterized by the 1st alloy powder and the 2nd alloy powder being mixed by the predetermined presentation.

[Claim 14] Rare earth alloy powder according to claim 13 characterized by the weight ratio of Cu and Co being $Cu/Co=0.02-0.2$.

[Claim 15] Rare earth alloy powder according to claim 13 characterized by the 2nd alloy powder being mixed with two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, and the 1st alloy coarse powder with which the amounts of boron B differ in a list by the predetermined presentation.

[Claim 16] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, The alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu) is used as the 2nd alloy aluminum0.01 - 2.0mass%. The manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 17] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, aluminum0.01 - 2.0mass%, Remainder Fe (a part of Fe is permuted by Co and Cu) The manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy with which the weight ratio of Cu and Co consists of $Cu/Co=0.02-0.2$, and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 18] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, It is the alloy which consists of the remainder Fe, the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, The alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu) is used as the 2nd alloy aluminum0.01 - 2.0mass%. The manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with

which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 19] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Rare earth alloy powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu) less than [boron B0.8mass%] and aluminum0.01 - 2.0mass%, and is characterized by the 1st alloy powder and the 2nd alloy powder being mixed by the predetermined presentation.

[Claim 20] Rare earth alloy powder according to claim 19 characterized by the weight ratio of Cu and Co being $Cu/Co=0.02-0.2$.

[Claim 21] Rare earth alloy powder according to claim 19 characterized by the 2nd alloy powder being mixed with two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, and the 1st alloy coarse powder with which the amounts of boron B differ in a list by the predetermined presentation.

[Claim 22] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Less than [boron B0.8mass%], aluminum0.01 - 2.0mass%, The manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 23] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which

consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Less than [boron B0.8mass%], aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe (a part of Fe is permuted by Co and Cu, and the weight ratio of Cu and Co is $Cu/Co=0.02-0.2$) is used as the 2nd alloy. The manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Claim 24] R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, It is the alloy which consists of the remainder Fe, the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Less than [boron B0.8mass%], aluminum0.01 - 2.0mass%, The manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[Translation done.]

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[The technical field to which invention belongs] This invention relates to the alloy powder for R-T-B (for rare earth and T, B, such as transition metals, is [R] boron) system permanent magnets, and the manufacture approach of a R-T-B system permanent magnet of having used this.

[0002]

[Description of the Prior Art] A R-T-B system permanent magnet is used in broad fields, such as various home electronics, information communication equipment, computer-related peripherals, and various motors, and magnetic properties, thermal resistance, and the further corrosion resistance improvement are desired also for the magnet used today to compensate for the miniaturization of these product groups, improvement in the speed, and expansion of an operating environment.

[0003] A R-T-B system permanent magnet dissolves a raw material alloy, it grinds the obtained ingot, fabricates it, sinters it, heat-treats it, it processes it, and is manufactured. Although wet grinding which used the ball mill etc. is also possible for grinding, jet mill grinding using inactive high pressure gas is common. Thus, since the fines obtained are activity very much, stabilization is attained or the method of mixing the oxygen of a minute amount in the grinding air current of a jet mill, and collecting fines to straight mineral oil etc. is taken. shaping performed all over a magnetic field -- dry pressing and a wet compaction -- all are used. As for the sintered compact which sintering was performed in a vacuum or inert gas in the 1000 degrees C - 1150 degrees C temperature requirement, and was subsequently obtained, it is common to perform heat treatment of 1 time or

multiple times at suitable temperature.

[0004] Although the R-T-B system permanent magnet had the problem that corrosion resistance and thermal resistance were low at the beginning, it has been remarkably improved by development of coating techniques, such as examination of an alloying element and plating. Moreover, the corrosion-resistant improvement of the magnet material itself is also very important when raising the dependability after coating, and various alloying elements are examined.

Generally elements, such as Co and Dy, are used as these alloying elements. Co improves corrosion resistance by raising Curie temperature, and improving the temperature characteristic, and using R rich phase as an R_3Co intermetallic compound. Dy raises coercive force by making the anisotropy field H_A of the main phase increase. Furthermore, additional trace elements, such as Cu, Ga, and aluminum, are also used. By carrying out compound addition with Co, Cu extends the optimal heat treatment range, and contributes to the improvement in coercive force (JP,1-219143,A). Moreover, it is known that a grain boundary phase will become a R-Co-Cu intermetallic compound by addition of Cu, and corrosion resistance will increase further compared with the case of only Co addition. It is known that alloying elements, such as Ga and aluminum, also have effectiveness in improvement in coercive force.

[0005] As the addition approaches, such as Co, Dy, and Cu, one so-called alloying method added in the dissolution phase of a raw material alloy and two alloying methods (alligation) which mix the alloy of a predetermined presentation after coarse grinding or pulverizing are used. the element contributed to corrosion resistance, such as Co and Dy, for the purpose of powdered antioxidizing in two alloying methods -- R -- it is shown by by adding into a rich alloy and using R rich alloy as an intermetallic compound with the specific crystal structure especially that the oxidation resistance of alloy powder increases (JP,5-182813,A -182816). Moreover, it means centralizing elements contributed to improvement in coercive force, such as Cu, aluminum, and Ga, on a grain boundary phase, and the approach of adding these elements to R rich alloy side

is shown.

[0006]

[Problem(s) to be Solved by the Invention] Although addition of Co, Dy, Cu, etc. has effectiveness in corrosion resistance and a heat-resistant improvement, if Co and Cu are added when one alloying method is used, it will set in few presentation regions of Dy where a high residual magnetic flux density is demanded, The grain growth at the time of sintering tends to take place, and it is in the inclination for big and rough crystal grain to appear mostly. Consequently, the particle size distribution of the main phase crystal grain of a sintered compact became large, and there was a problem of being easy to cause the fall of coercive force and square shape nature. Moreover, the following troubles will be got if they tend to carry this out on a scale of mass production, although two alloying methods are very attractive approaches from a viewpoint of high-performance-izing. That is, the main phase alloy with few amounts of rare earth and the so-called R rich alloy which was rich in rare earth must be prepared, and large modification of a raw material alloy system is called for. Moreover, it not only must carry out separate optimization of each grinding condition, but a process will become complicated when the main phase alloy and R rich alloy need modification of coarse-grinding conditions since hydrogen absorption properties differ, and R rich alloy tends to disperse when carrying out jet mill grinding of the mixed coarse powder, since pulverizing nature differs, and mixing after pulverizing.

[0007] In the approach of adding Co, Cu, Dy, etc., it can utilize enough, without changing the conventional amount raw material alloy of rare earth in any way, and this invention does not invite generating of the big and rough crystal grain at the time of sintering, and the fall of coercive force, but aims at offering the manufacture approach of the alloy powder for R-T-B system permanent magnets which can attain high magnetic properties, and a R-T-B system permanent magnet.

[0008]

[Means for Solving the Problem] This invention makes the following configuration main point, in order to solve the above-mentioned technical problem. In addition, following the (1) - (6) is the case where the boron B addition of the 2nd alloy is substantially made into zero using the compound addition effectiveness of Ga and aluminum. Following the (7) - (12) is the case where the boron B addition of the 2nd alloy is made into less than [0.8mass%] using the compound addition effectiveness of Ga and aluminum. Moreover, following the (13) - (18) is the case where carried out independent addition of the aluminum and the boron B addition of the 2nd alloy is substantially made into zero. Following the (19) - (24) is the case where carried out independent addition of the aluminum and the boron B addition of the 2nd alloy is made into less than [0.8mass%].

(1) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B 0.8 - 1.2mass%. Ga 0.01 - 0.5mass% and aluminum 0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga 0.01 - 0.5mass% and aluminum 0.01 - 2.0mass%, It is the rare earth alloy powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by the 1st alloy powder and the 2nd alloy powder being mixed by the predetermined presentation.

(2) It is the rare earth alloy powder given in (1) characterized by the weight ratio of Cu and Co being $Cu/Co=0.02-0.2$.

(3) said -- R -- inside -- heavy rare earth -- a content -- differing -- the -- one -- an alloy -- coarse powder -- a list -- boron -- B -- an amount -- differing -- the -- one -- an alloy -- coarse powder -- the -- one -- an alloy -- powder -- two -- a sort -- more than -- the -- two -- an alloy -- powder -- predetermined -- a presentation -- mixing -- having -- **** -- things -- the description -- ** -- carrying out -- (-- one --) -- a publication -- a rare earth alloy -- powder -- it is .

(4) R(at least one or more sorts of rare earth elements containing Y) 29 -

33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(5) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe (a part of Fe is permuted by Co and Cu, and the weight ratio of Cu and Co is $Cu/Co=0.02-0.2$) is used as the 2nd alloy. It is the manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(6) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the alloy which consists of the remainder Fe, the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B

differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(7) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than [boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the rare earth alloy powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by the 1st alloy powder and the 2nd alloy powder being mixed by the predetermined presentation.

(8) It is the rare earth alloy powder given in (7) characterized by the weight ratio of Cu and Co being Cu/Co=0.02-0.2.

(9) said -- R -- inside -- heavy rare earth -- a content -- differing -- the -- one -- an alloy -- coarse powder -- a list -- boron -- B -- an amount -- differing -- the -- one -- an alloy -- coarse powder -- the -- one -- an alloy -- powder -- two -- a sort -- more than -- the -- two -- an alloy -- powder -- predetermined -- a presentation -- mixing -- having -- **** -- things -- the description -- ** -- carrying out -- (-- seven --) -- a publication -- a rare earth alloy -- powder -- it is .

(10) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy

which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than [boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(11) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than [boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe (a part of Fe is permuted by Co and Cu, and the weight ratio of Cu and Co is $Cu/Co=0.02-0.2$) is used as the 2nd alloy. It is the manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(12) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of Ga and the aluminum is carried out boron B0.8 - 1.2mass%. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, The 1st alloy coarse powder with which it is the alloy which consists of the remainder Fe, and the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Compound addition of less than

[boron B0.8mass%], and Ga and aluminum is carried out. Ga0.01 - 0.5mass% and aluminum0.01 - 2.0mass%, It is the manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(13) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, It is the rare earth alloy powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by the 1st alloy powder and the 2nd alloy powder being mixed by the predetermined presentation aluminum0.01 - 2.0mass%.

(14) It is the rare earth alloy powder given in (13) characterized by the weight ratio of Cu and Co being Cu/Co=0.02-0.2.

(15) said -- R -- inside -- heavy rare earth -- a content -- differing -- the -- one -- an alloy -- coarse powder -- a list -- boron -- B -- an amount -- differing -- the -- one -- an alloy -- coarse powder -- the -- one -- an alloy -- powder -- two -- a sort - - more than -- the -- two -- an alloy -- powder -- predetermined -- a presentation -- mixing -- having -- **** -- things -- the description -- ** -- carrying out -- (-- 13 --) -- a publication -- a rare earth alloy -- powder -- it is .

(16) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, The alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu) is used as the 2nd alloy aluminum0.01 - 2.0mass%. It is the manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with

which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(17) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, aluminum0.01 - 2.0mass%, Remainder Fe (a part of Fe is permuted by Co and Cu) It is the manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy with which the weight ratio of Cu and Co consists of $Cu/Co=0.02-0.2$, and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(18) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, It is the alloy which consists of the remainder Fe, the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, The alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu) is used as the 2nd alloy aluminum0.01 - 2.0mass%. It is the manufacture approach of the rare earth permanent magnet characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(19) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, It is the rare earth alloy

powder which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by the 1st alloy powder and the 2nd alloy powder being mixed by the predetermined presentation less than [boron B0.8mass%] and aluminum0.01 - 2.0mass%.

(20) It is the rare earth alloy powder given in (19) characterized by the weight ratio of Cu and Co being $Cu/Co=0.02-0.2$.

(21) said -- R -- inside -- heavy rare earth -- a content -- differing -- the -- one -- an alloy -- coarse powder -- a list -- boron -- B -- an amount -- differing -- the -- one -- an alloy -- coarse powder -- the -- one -- an alloy -- powder -- two -- a sort - - more than -- the -- two -- an alloy -- powder -- predetermined -- a presentation -- mixing -- having -- **** -- things -- the description -- ** -- carrying out -- (-- 19 --) -- a publication -- a rare earth alloy -- powder -- it is .

(22) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Less than [boron B0.8mass%], aluminum0.01 - 2.0mass%, It is the manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(23) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe is used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Less than [boron B0.8mass%], aluminum0.01 - 2.0mass%, The alloy which consists of the remainder Fe (a part of Fe is permuted by Co and Cu, and the weight ratio of Cu and Co is $Cu/Co=0.02-0.2$) is used as the 2nd alloy. It is the manufacture approach of the rare earth permanent magnet characterized by fabricating the

rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

(24) R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Boron B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, It is the alloy which consists of the remainder Fe, the 1st alloy coarse powder with which the contents of heavy rare earth differ among said R, Two or more sorts of the 1st alloy powder of the 1st alloy coarse powder with which the amounts of boron B differ in a list are used as the 1st alloy. R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, Less than [boron B0.8mass%], aluminum0.01 - 2.0mass%, It is the manufacture approach of the rare earth permanent magnet which uses as the 2nd alloy the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and is characterized by fabricating the rare earth alloy powder with which the 1st alloy powder and the 2nd alloy powder were mixed by the predetermined presentation all over a magnetic field, and subsequently sintering it.

[0009] (Operation) As a means to solve the above-mentioned trouble, this invention can be set to two alloying methods. As a result of examining the addition approach of Co, Cu, Dy, and B, and the amount of rare earth, Co, Use alloy coarse powder of the amount of rare earth as the 1st alloy conventionally which does not contain Cu, and the amount of rare earth is fundamentally [as the 1st alloy] equal to this. By adding Co of a specific ratio, and Cu into the 2nd alloy fewer than the 1st alloy, excluding B substantially, and pulverizing and sintering after mixing such alloy coarse powder It can utilize enough, without changing the conventional amount raw material alloy of rare earth in any way, generating of the big and rough crystal grain at the time of sintering and the fall of coercive force are not invited, but it finds out that corrosion resistance, heat-resistant improvement, and high magnetic properties can be attained. Furthermore, it finds out that a quality governing can be easily performed only by changing a mixing ratio by the approach of mixing with the 2nd alloy two or more

alloy coarse powder with which presentations, such as Dy and B, differ.

[0010] This invention Namely, R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, The alloy which consists of the remainder Fe and an unescapable impurity is used as the 1st alloy aluminum0.01 - 2.0mass% B0.8 - 1.2mass%. With the 1st alloy, substantially The equal amount of R, less than [B0.8mass%], aluminum0.01 - 2.0mass%, It is the R-T-B system alloy powder with which the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and an unescapable impurity is used as the 2nd alloy, and the 1st alloy powder and the 2nd alloy powder are mixed by the predetermined presentation. Moreover, R(at least one or more sorts of rare earth elements containing Y) 29 - 33mass%, B0.8 - 1.2mass%, aluminum0.01 - 2.0mass%, Ga0.01 - 0.5mass%, The alloy which consists of the remainder Fe and an unescapable impurity is used as the 1st alloy. Substantially with the 1st alloy The equal amount of R, Less than [B0.8mass%], aluminum0.01 - 2.0mass%, Ga0.01 - 0.5mass%, It is the R-T-B system alloy powder with which the alloy which consists of the remainder Fe (what permuted a part of Fe by Co and Cu), and an unescapable impurity is used as the 2nd alloy, and the 1st alloy powder and the 2nd alloy powder are mixed by the predetermined presentation. Moreover, the weight ratio of Cu and Co is the above-mentioned R-T-B system alloy powder which is Cu/Co=0.02-0.2. Moreover, two or more sorts of 1st alloy powder with which the amounts of heavy rare earth differ, and the 2nd alloy powder are R-T-B system alloy powder currently mixed by the predetermined presentation. Furthermore, it is the manufacture approach of the R-T-B system permanent magnet which fabricates these R-T-B system alloy powder all over a magnetic field, and subsequently sinters it.

[0011]

[Embodiment of the Invention] In this invention, R is at least one or more sorts of the rare earth elements containing Y, and Nd, Pr, and its Dy are desirable. Also with Nd and Dy chisel, although it is good, the mixture of Nd and Pr may be used instead of Nd. Since a residual magnetic flux density will fall if it becomes poor

sintering R of the 1st alloy which serves as a subject since the liquid phase runs short less than [29mass%], and it exceeds 33mass%, an addition is made into 29mass(es)% - 33mass%. Less than [0.8mass%], since B rich phase which is a nonmagnetic phase will increase too much and a residual magnetic flux density will fall if coercive force decreases rapidly and 1.2mass% is exceeded, since R2T17 phase appears, B of the 1st alloy may be 0.8 - 1.2mass%. When adding aluminum, or aluminum and Ga into the 1st alloy, aluminum and the amount of Ga(s) are made into Ga0.01 - 0.5mass% aluminum0.01 - 2.0mass%. Although aluminum shows the effectiveness of the improvement in coercive force, if the effectiveness exceeds 2.0mass(es)% rather than is enough, the fall of a residual magnetic flux density is not greatly desirable [aluminum] less than [0.01mass%]. Although coercive force of Ga improves by the addition similarly, if less than [0.01mass%] is inadequate too as for the effectiveness and 0.5mass% is exceeded, while the effectiveness of the improvement in coercive force will be saturated, a residual magnetic flux density falls. It is more effective if Ga and aluminum carry out compound addition in this invention.

[0012] Although R of the 2nd alloy is fundamentally made equal to the 1st alloy, you may shift somewhat with convenience, lot variation, etc. of alloy supply. The presentation range is made into R29 - 33mass% equally to the 1st alloy. More than at 0.8mass%, the effectiveness which controls generating of a big and rough grain becomes small, and the amount of B of the 2nd alloy causes reduction in coercive force, and aggravation of square shape nature. Therefore, although considered as less than [0.8mass%], B is not added preferably. Although Ga of the 2nd alloy and aluminum are fundamentally made equal to the 1st alloy, you may shift somewhat with convenience, lot variation, etc. of alloy supply. When adding aluminum, or aluminum and Ga, the presentation range is made into Ga0.01 - 0.5mass% aluminum0.01 - 2.0mass% equally to the 1st alloy. In addition, it is more effective if Ga and aluminum carry out compound addition in this invention. Co of the 2nd alloy and especially the addition of Cu cannot be limited, but can be set up from the relation between the addition in the last

presentation, and a compounding ratio, and the addition in the last presentation can be set up according to an application and the purpose. the compounding ratio of the 2nd alloy [as opposed to the 1st alloy on the other hand] -- 1st alloy: -- the 2nd -- especially as for limitation, this is not carried out, either, although alloy =99:1-70:30 are desirable.

[0013] If the weight ratio of Cu and Co has the small effectiveness which extends the heat-treatment-temperature range as Cu/Co is less than 0.02 and exceeds 0.2, Co will cause the fall of a residual magnetic flux density, and the fall of square shape nature in the very general presentation which is about 2mass%. Therefore, it is referred to as Cu/Co=0.02-0.2.

[0014] The 1st alloy coarse powder in this invention is not restricted to the thing of a single presentation. That is, to these [the 1st alloy coarse powder with which the amounts of heavy rare earth, such as Dy and Tb, differ, the 1st alloy coarse powder with which the amounts of B differ further and] two or more sorts, the 2nd alloy coarse powder with which Co and Cu were added may be blended, and you may mix. In this case, adjustment of Dy or B can be easily performed only by changing a compounding ratio.

[0015]

[Example] Hereafter, the concrete example of this invention is shown and the contents of this invention are explained to a detail.

(Example 1) The alloy which consists of the remainder Fe was cast in the strip cast method aluminum0.07mass% B1.0mass% Pr7.0mass% Nd25.3mass%. After inserting this alloy in the processing container and performing heat treatment of 1000 degree-Cx2h in a vacuum, it cracked by the hydrogen absorption method and considered as raw material coarse powder (a Table 1 publication, Alloy A). Moreover, the alloy which consists of the remainder Fe was similarly used as raw material coarse powder aluminum0.07mass% Cu1mass% Co20mass% Dy8.5mass% Pr5.2mass% Nd18.6mass% (a Table 1 publication, Alloy I). Two kinds of this alloy coarse powder was thrown into the V shaped rotary mixer at an alloy I10mass% rate alloy A90mass%, and it mixed for 15

minutes. This mixed coarse powder was ground so that it might become the mean particle diameter of 4.7 micrometers with the jet mill using nitrogen high pressure gas. It fabricated by the pressure of 1.0 Ton/cm², carrying out orientation of the obtained mixed fines all over the magnetic field of 0.6 MA/m. The acquired Plastic solid performed sintering of 1060-degree-C, 1080-degree-C, or 1100 degree-Cx 2 hours in the vacuum. Subsequently, these sintered compacts performed heat treatment of 480 more degree-Cx 1 hour, after performing heat treatment of 900 degree-Cx 1 hour in Ar ambient atmosphere. Magnetic properties were measured after observing the appearance of a sintered compact. The result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. The value with good magnetic properties was acquired, sintering temperature is 1100 degrees C at this time, and the big and rough grain etc. was not seen.

[0016] (Example 1 of a comparison) Cu0.1mass%, aluminum0.07mass%, the alloy which consists of the remainder Fe was cast in the strip cast method, and grinding, sintering, and heat treatment were performed like the example 1 Co2mass% B0.9mass% Dy0.85mass% Pr6.85mass% Nd24.6mass% which is the last presentation of this example. Magnetic properties are measured after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. Although the optimal sintering temperature was 1080 of 1060 degrees C, 1080 degrees C, and 1100 degrees C, H_{cj} was lower than the example 1, and the big and rough grain was observed. Moreover, sintering of the 1060-degree C sample was clearly insufficient.

[0017] (Example 2 of a comparison) Coarse grinding was carried out like the example 1 using Alloy R and Alloy S which were shown in Table 1, and pulverizing, sintering, and heat treatment were performed after mixing so that it might become the last presentation. Here, Co and Cu were uniformly added into both alloys, and Dy was added into Alloy S. Magnetic properties are measured

after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. Hcj was lower than the example 1, and the big and rough grain was observed.

[0018] (Example 3 of a comparison) Coarse grinding was carried out like the example 1 using Alloy C and Alloy Q which were shown in Table 1, and pulverizing, sintering, and heat treatment were performed after mixing so that it might become the last presentation. Here, Dy, Co, and Cu were added into Alloy Q, and B added both alloys uniformly. Magnetic properties are measured after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. Hcj was lower than the example 1, and the big and rough grain was observed although it was fewer than the examples 1 and 2 of a comparison.

[0019] (Example 2) Coarse grinding was carried out like the example 1 using Alloy A and Alloy K which were shown in Table 1, and pulverizing, sintering, and heat treatment were performed after mixing so that it might become the last presentation. Here, Dy, Co, and Cu were added into Alloy K, and B could be 0.4mass(es)%. Alloy K is the 2nd alloy of this invention. Magnetic properties are measured after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. The good value was acquired by magnetic properties like the example 1, sintering temperature is 1100 degrees C at this time, and the big and rough grain etc. was not seen.

[0020] (Example 3) Coarse grinding was carried out like the example 1 using Alloy A and Alloy L which were shown in Table 1, and pulverizing, sintering, and heat treatment were performed after mixing so that it might become the last presentation. Here, Dy, Co, and Cu were added into Alloy L, and B could be 0.7mass(es)%. Alloy L is the 2nd alloy of this invention. Magnetic properties are

measured after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. The good value was acquired by magnetic properties like the example 1, sintering temperature is 1100 degrees C at this time, and the big and rough grain etc. was not seen.

[0021] (Example 4) Coarse grinding was carried out like the example 1 using Alloy B, Alloy C, and Alloy I which were shown in Table 1, and pulverizing, sintering, and heat treatment were performed after mixing so that it might become the last presentation. Here, Dy, Co, and Cu were added into Alloy I, and B was taken as additive-free. Alloy I is the 2nd alloy of this invention. Magnetic properties are measured after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. The good value was acquired by magnetic properties like the example 1, sintering temperature is 1100 degrees C at this time, and the big and rough grain etc. was not seen.

[0022] (Example 5) Coarse grinding was carried out like the example 1 using Alloy B, Alloy C, Alloy D, and Alloy J which were shown in Table 1, and pulverizing, sintering, and heat treatment were performed after mixing so that it might become the last presentation. Here, Co and Cu were added into Alloy J and B was taken as additive-free. Alloy J is the 2nd alloy of this invention. Dy was added with the alloy D which is one of the 1st alloy of this invention. Magnetic properties are measured after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. The good value was acquired by magnetic properties like the example 1, sintering temperature is 1100 degrees C at this time, and the big and rough grain etc. was not seen.

[0023] (Example 4 of a comparison) Coarse grinding was carried out like the

example 1 using Alloy T and Alloy U which were shown in Table 1, and pulverizing, sintering, and heat treatment were performed after mixing so that it might become the last presentation. here -- Dy, Co, and Cu -- R -- it added into the rich alloy U and B was taken as additive-free. Alloy U is not the 2nd alloy of this invention. Magnetic properties are measured after observing the appearance of the obtained sintered compact, and the result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 1. The good value was acquired by magnetic properties like the example 1, sintering temperature is 1100 degrees C at this time, and the big and rough grain etc. was not seen. This result shows that the magnetic properties acquired in the examples 1-5 are equivalent to two conventional alloying methods (example 4 of a comparison).

[0024] (Examples 6-10, examples 5-8 of a comparison) the -- one -- an alloy -- A-D -- the -- two -- an alloy -- I-L -- a comparison -- ** -- an alloy -- P-U -- a presentation -- setting -- Ga -- 0.1 -- mass(es) -- % -- having added -- an alloy -- new -- producing -- the -- one -- an alloy -- A -- ' - D -- ' -- the -- two -- an alloy -- I -- ' - L -- ' -- a comparison -- ** -- an alloy -- P -- ' - U -- ' -- ** -- having carried out . The sintered compact was produced by the same approach as examples 1-5 and the examples 1-4 of a comparison, and magnetic properties were measured after observing the appearance of a sintered compact. The result of magnetic properties when square shape nature is the highest, sintering temperature, and appearance observation is shown in Table 2. About the optimal sintering temperature and the appearance of a big and rough grain, although it is the same as that of the result of Table 1, it can check that the level of Hcj carries out improvement in 0.2 MA/m extent. The compound addition effectiveness of Ga has shown up.

[0025]

[Table 1]

		組 成 (mass%)							
		Nd	Pr	Dy	TRE	B	Co	Cu	Fe
第1 合金	A	25.3	7.0	0	32.3	1.00	0	0	bal.
	B	25.2	7.0	0	32.2	1.07	0	0	bal.
	C	25.3	7.0	0	32.3	0.90	0	0	bal.
	D	11.9	3.3	17.0	32.2	1.07	0	0	bal.
第2 合金	I	18.6	5.2	8.5	32.3	0	20	1	bal.
	J	25.3	7.0	0	32.3	0	20	1	bal.
	K	20.8	5.7	5.7	32.2	0.4	13.3	0.67	bal.
	L	23.1	6.4	2.8	32.3	0.7	6.7	0.34	bal.
比較 合金	P	24.6	6.85	0.85	32.3	0.90	2	0.1	bal.
	Q	18.5	5.2	8.5	32.2	0.90	20	1	bal.
	R	25.3	6.9	0	32.2	0.90	2	0.1	bal.
	S	12.0	3.3	17.0	32.3	1.07	2	0.1	bal.
	T	23.8	6.6	0	30.4	1.03	0	0	bal.
	U	30.1	8.4	7.2	45.7	0	16.9	0.85	bal.
最終組成		24.6	6.85	0.85	32.3	0.90	2	0.1	bal.

Al:0.06~0.08mass%

	配合(合金×配合率)	Br (T)	Hcj (MA/	Hk/Hc (%)	最適焼 温度	粗大粒 外観
実施例	A×0.9+I×0.1	1.36	1.17	98.3	1100	○
比較例	P	1.35	1.01	98.1	1080	×
比較例	R×0.95+S×0.05	1.35	1.0	98.2	1080	×
比較例	C×0.9+Q×0.1	1.35	1.03	98.1	1080	△
実施例	A×0.85+K×0.15	1.35	1.16	98.0	1100	○
実施例	A×0.7+L×0.3	1.36	1.16	97.8	1100	○
実施例	B×0.53+C×0.37+I×0.1	1.35	1.17	98.2	1100	○
実施例	B×0.5+C×0.35+D×0.05+J	1.36	1.17	98.4	1100	○
比較例	T×0.88+U×0.12	1.36	1.18	98.1	1100	○

○:なし △:あり ×:多し

[0026]

[Table 2]

	配合(合金×配合率)	Br (T)	Hcj (MA/	Hk/Hc (%)	最適焼 温度	粗大粒 外観
実施例	A'×0.9+I'×0.1	1.35	1.38	98.4	1100	○
比較例	P'	1.34	1.21	97.9	1080	×
比較例	R'×0.95+S'×0.05	1.35	1.22	97.9	1080	×
比較例	C'×0.9+Q'×0.1	1.35	1.25	98.4	1080	△
実施例	A'×0.85+K'×0.15	1.35	1.37	98.2	1100	○
実施例	A'×0.7+L'×0.3	1.35	1.35	98.1	1100	○
実施例	B'×0.53+C'×0.37+I'×0.1	1.35	1.38	98.4	1100	○
実施例	B'×0.5+C'×0.35+D'×0.05+	1.36	1.37	98.4	1100	○
比較例	T'×0.88+U'×0.12	1.35	1.38	98.4	1100	○

○:なし △:あり ×:多し

[0027]

[Effect of the Invention] According to this invention, in the approach of adding Co, Cu, Dy, etc., it can utilize enough, without changing the raw material alloy of the

conventional amount of rare earth in any way, generating of the big and rough crystal grain at the time of sintering and the fall of coercive force cannot be invited, but high magnetic properties can be attained.

[Translation done.]